

A non-hydrostatic SI dynamical core : current-state, limitations and perspectives

Pierre Bénard

(Thanks to: F. Voitus, S. Caluwaerts, Ch. Colavolpe, Y. Seity, ...)

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Galaxy

We speak about the dynamical core of the following “galaxy” :
IFS(ECMWF) / ARPEGE (MF) / ALADIN (Int'l) / HARMONIE (Int'l)

The dynamical core of these models share many parts in common,
developed jointly, code cooperation

History (dynamical core)

- IFS+ARPEGE (Global HPE) oper
- ALADIN (LAM HPE) oper
- ALADIN NH (LAM NH) – HARMONIE, AROME... .. oper
- ARPEGE NH and IFS NH (Global NH) exper

INTRODUCTION

Three talks are dealing more or less with the same dynamical core (or research avenues) :

- N. Wedi
- P. Bénard (time)
- M. Hortal (space)

OUTLINE of the talk

- Current status of AROME model
- Limitations (mainly from SI point of view)
- Perspectives

CURRENT STATUS of AROME

What is AROME ?

- AROME: High resol LAM model NH (Euler Equations) operational at Meteo-France (also in some other countries)
- Dyn core IFS/ARP/ALA-NH (common concept, spectral SI SL)
- “Meso-scale” physics from 90-00’s research world (column-wise)
- 3D-VAR Data Assimilation with 3h cycle
- Many mesoscale observations assimilated (Radar reflectivities, Doppler wind, thinner Sat radiances...)

Current oper configuration of AROME

- $\Delta x = 2.5$ km, 60 levels, 750*720 points
- $\Delta t = 60$ s (30h forecasts)
- limited overcost with respect to HPE version

CURRENT STATUS of AROME

Experimental version (1)

- $\Delta x = 1.3$ km, 90 levels, $\Delta t = 45$ s
- Prototype for next oper version
- smaller domain, dynamical adaptation (no Data Assim)
- Has run routinely at 00UTC \rightarrow 30h for one year
- robust, positive impact, nice results

Experimental version (2)

- $\Delta x = 0.5$ km, ~ 100 levels, Δt 10-15s
- Only isolated test cases (in dynamical adaptation)
- \rightarrow robustness OK (but small sample)

Next operational configuration of AROME

Characteristics

- $\Delta x = 1.3$ km, 90 levels, 1536*1440 points
- $\Delta t = 45$ s (still 30h forecasts)

CPU overcost to current version

| $\Delta x + \text{Dom}$ | Δz | Δt | SI \rightarrow ICI | Other | Total |
|-------------------------|--------------|---------------|----------------------|--------------|-------------|
| $\times 4.1$ | $\times 1.5$ | $\times 1.33$ | $\times 1.1$ | $\times 1.1$ | $\times 10$ |

Maximum slope : $23^\circ \rightarrow 38^\circ$ hence "SI \rightarrow ICI" .

On new Bull machine ~ 25000 cores (~ 1000 nodes) ~ 500 tflops
 \Rightarrow new AROME ($\Delta x = 1.3$ km) in operations at summer 2014.

Limitations of the current system

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Identified concerns

- Scalability (mainly at high granularity)
- Ability to manage severe high-resolution flows and slopes
- Compatibility with new developments (e.g. change progn. var., Vertical Finite Elements,...)

Possible modifications (of time-scheme) for solutions

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Retained option for mid-term: improve SI scheme

Original spirit of SI Schemes

System to solve (e.g. in Leap-Frog)

$$\frac{\partial X}{\partial t} = M(X) \quad \rightarrow \quad \frac{X^+ - X^-}{2\Delta t} = RHS$$

Two limiting-case of centered time schemes

- Explicit : $\frac{X^+ - X^-}{2\Delta t} = M(X^0)$
→ easy, bad stability (wave-CFL)
- Crank-Nicolson: $\frac{X^+ - X^-}{2\Delta t} = M\left(\frac{X^+ + X^-}{2}\right)$
→ very good stability, but very difficult to attain

Original spirit of SI Schemes

Original SI scheme (1970s)

Choose a simple stationary fixed state X_*

Define the linear operator L_* as $L_* = \left. \frac{\partial M}{\partial X} \right|_{X_*}$

Then SI scheme:

$$\frac{X^+ - X^-}{2\Delta t} = [M - L_*](X^0) + L_* \left(\frac{X^+ + X^-}{2} \right)$$

$$X^+ = (I - \Delta t L_*)^{-1} \{ X^- + \Delta t [2M(X^0) + (L_* X^- - 2L_* X^0)] \}$$

Stability depends on what is in $[M - L_*]$

and may lead to bad surprises...

"General pedagogy" about SI Schemes

- Stable explicit schemes are conditionally stable (in terms of Δt), CFL...

Analysis for simple flows :

SI schemes may be unconditionally stable (in terms of Δt)

e.g. handbooks : "... SI-SL unconditionally stable ... "

Ignoring SI overcost

"I'm going to add a SI scheme in my model,
putting some implicitness in the scheme cannot hurt..."

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This is wrong !

- SI schemes may be unconditionally unstable (in terms of Δt)
- 'unstable' SI schemes are unconditionally unstable (in terms of Δt)

"SI Schemes

Robustness of simple SI schemes becomes poorer and poorer when the stiffness of the system increases:

SW → HPE → EE → EE + High Resolution

If SI kept, need to improve it (from the original idea)

Two main ways:

“TL-SI” Schemes

Improving the content of L_*

If we define $X_* = X^0$ (X at current time-step)

The linear operator L_* is then $L_0 = \left. \frac{\partial M}{\partial X} \right|_{X_0}$ (same TL as in 4D-VAR)

Then SI scheme:

$$\frac{X^+ - X^-}{2\Delta t} = [M - L_0](X^0) + L_0 \left(\frac{X^+ + X^-}{2} \right)$$

Very close to Crank-Nicolson, need to invert L_0 ($I - \Delta t L_0$, indeed)

But L_0 is large 3D, non-sparse, time-dependant, and ill-conditioned
solution approached by iterative solver operator of the size of X

Not very realistic (4D-VAR uses TL, but does not try to invert it)

Practical approach : drop as much as possible terms or dependencies in L_0
while trying to remain stable

Instability usually occur by lack of convergence toward the aimed scheme
in the iterative solver.

"ICI" Schemes

Improve by iterating L_*

Define a time-independent linear operator L_*

Then use iterative scheme (with iterator index k):

$$\frac{X^{+(k)} - X^-}{2\Delta t} = M\left(\frac{X^{+(k-1)} + X^-}{2}\right) + L_*\left(\frac{X^{+(k)} - X^{+(k-1)}}{2}\right)$$

Initialize by a simple extrapolated estimate: $X^{+(0)} = (2X^0 - X^-)$

$k = 1 \rightarrow$ classical SI scheme

$$\frac{X^+ - X^-}{2\Delta t} = M\left[\frac{(2X^0 - X^-) + X^-}{2}\right] + L_*\left[\frac{X^+ - (2X^0 - X^-)}{2}\right]$$

then $k = 2, k = 3, \dots \rightarrow$ ICI scheme

If converging, converges toward Crank-Nicolson scheme

Pre-inversion \Rightarrow still relatively cheap (if k_{\max} small)

If L_* too simple, will not lead to a convergent system

These are not the same

$$\frac{X^+ - X^-}{2\Delta t} = [M - L_*](X^0) + L_* \left(\frac{X^+ + X^-}{2} \right)$$

- TL-SI tries to minimize $L_* - L_{X_0}$
(to treat explicitly only the NL part of M)
- ICI tries to approach Crank-Nicolson globally
(to treat explicitly nothing)
- Both can always be combined

Limitations of the current AROME SI scheme

- Spectral: very efficient SI (direct solver), **but:**
- Spectral SI \Rightarrow Constant Coefficients SI (CCSI)
coefficients of L_* must not depend on space
otherwise no longer (direct) solution of SI problem

Example SW:

$$(I - \Delta t^2 \phi_* \nabla^2) \phi^+ = \text{RHS}$$

$$(I - \Delta t^2 \phi_*(x) \nabla^2) \phi^+ = \text{RHS}$$

- Slopes increase with resolution \rightarrow CCSI not robust enough:
 - $\Delta x = 2.5$ km: CCSI robust with $\Delta t = 60$ s
 - $\Delta x = 1.3$ km: CCSI not fully robust with $\Delta t = 30$ s
 - $\Delta x = 1.3$ km: CC ICI robust with $\Delta t = 45$ s (one iteration $k = 2$)

Still OK (with ICI) – even 30% cheaper – but indicates danger

Prioritizing identified concerns

- Scalability:
We think we can survive at mid-term (FLT,...)
- Compatibility with new developments:
We have now good hope to manage implementing VFEs
- Severe flows and slopes:
Is prioritized as the main concern at mid-term

PERSPECTIVES for our dynamical core

Postulates

- Assume the current SI scheme is operational-proof at $\Delta x \sim 500\text{m}$ (accuracy of the response, ability to include processes, scalability)
 - Assume (or show) that future potential problems first originate from the orographic forcing
-
- Concentrate on including orographic forcing terms in the SI scheme (only)
 - Try to keep the time-independent SI inversion problem pre-computed

PERSPECTIVES for our dynamical core

Include the orographic forcing into the SI treated terms

- SI problem remains time-independent by nature
- SI problem no longer homogeneous linear, non-separable
→ requires a 3D non-direct solver
- Strong identity required between space operators used in **explicit** RHS and in **implicit** LHS (to be inverted).

$$(u^+ + \Delta t \partial_x) T^+ = \dots + \Delta t \partial_x (2T^0 - T^-)$$

- Non-possible choice: spectral computation of derivatives in **explicit** terms and grid-point operators in the **matrix of the implicit scheme**
- Matrix form of spectral ∂_x possible but → many full blocks non-sparse 3D SI problem, not realistic (although time-independent)
- Non-spectral model / local horizontal operators only (preserve sparsity).
⇒ Horizontal: high-order FE

Consequences of non-spectral model

- Make the use of the solver compatible with efficiency/scalability
Choose solver which exploits sparse matrix property
- Which variables and staggering for horizontal FE ? (next slide)
- For global model, which grid geometry for horizontal FE (next slide)
- Preserve pre-computation SI operator ???

Which variables and staggering for horizontal FE ?

- Deals with short gravity waves propagation, geostrophic adjustment and computational modes
- Advantages of non-staggered grids:
 - Approach valid on any grid-geometry (i.e. problem of discretisation disconnected from the one of the geometry)
 - Preserve $(u+v):p$ d.o.f. ratio for no spurious computational modes (ratio 2:1 ensures only 2 gravity modes for one Rossby mode)
- Examine non-staggered grid with Vor-Div variables:
 - correct propagation of short gravity waves
 - needs transform $(VOR, DIV) \rightarrow (u, v)$ (Poisson Equation)
 - non-locality reappears, however standard and 2D problem ...
- PhD work by S. Caluwaerts (IRM - Brussels)

PERSPECTIVES for our dynamical core

Which grid-geometry for global horizontal FE ?

Deals with spurious evolution of Rossby waves

Reduced lat-lon grids

- Reported drawback: distorted Rossby waves propagation with spurious meridional transport
 - ... but this is only only for 40 years-old configurations
 - ... with 2nd-order FD schemes, with very low resolutions
 - ... and drastic grid-reduction
- Preserves simple geometry along each parallel circle
 - $(\partial/\partial\lambda)$: trivial 1D uniform spacing
 - $(\partial/\partial\varphi)$: uniform spacing
- Preserves existing model architecture

Further perspectives (not discussed)

- explore horizontally explicit schemes (HEVI) for EE
coupled with time-splitting technique
use with a pre-computed vertical SI scheme
sensitivity to the choice of the variable
(Phd work by Ch. Colavolpe)
- explore non-terrain-following coordinate with 'step-orography'
for very high resolution ('kick' response at orography-steps become evanescent?)

CONCLUSIONS

CONCLUSIONS

- Current SI scheme may reach its viability limits at some mid-term
- However still very competitive \Rightarrow mid-term-strategy :
change space-discretization (FE) and keep (improved) SI scheme
- Try to keep unmodified the deepest architectural nucleus of the model's kernel: grid A + lat-lon (reduced)
- This step is compatible with longer-term programs (HEVI,...)